

# Puzzle: 3D Nonlinear model of the vertical spring force of a trampoline - Can mathematical approximations be compensated through curve fitting ?

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The trampoline bed of Fig. 1 is deflected at the centre through a vertical force  $F$ . The amount of vertical deflection is  $d$ . To calculate its mathematical model we use the force vector diagrams of the longitudinal-sectional view  $LL'$  in Fig. 2 and in the cross-sectional view  $BB'$  in Fig. 3.

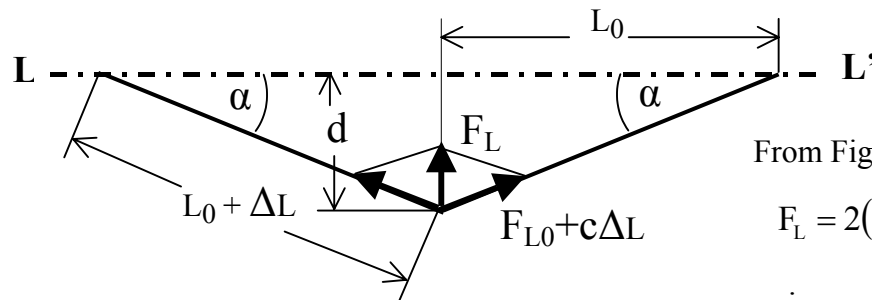
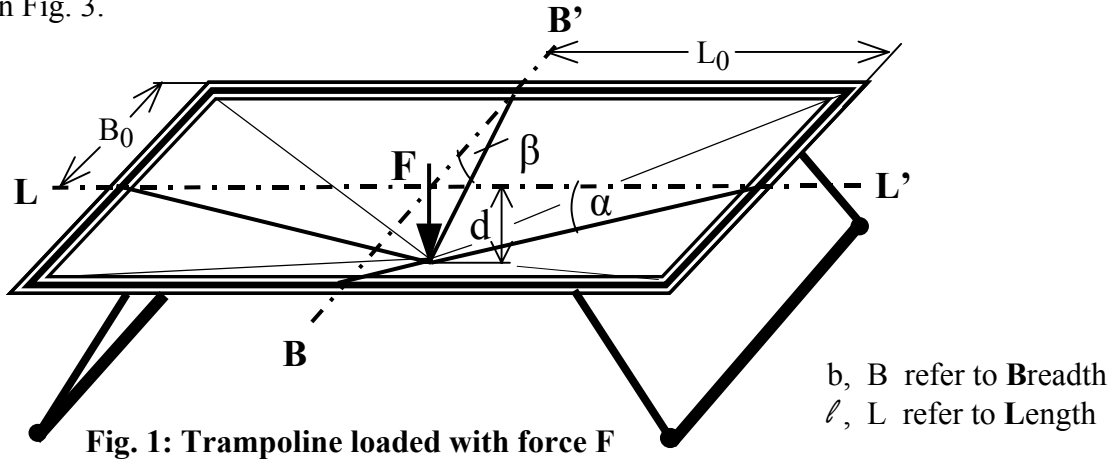


Fig. 2: Longitudinal-sectional view  $LL'$

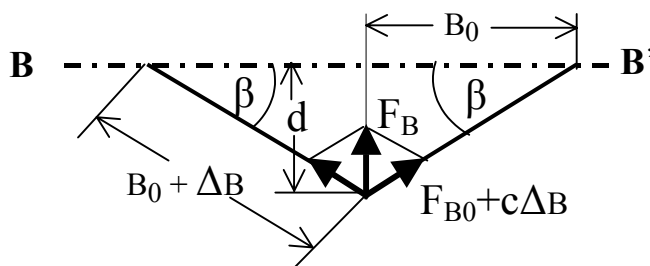


Fig. 3: Cross-sectional view  $BB'$

- $c$  = effective spring constant
- $L_0, B_0$  = half length/breadth of the tramp
- $\Delta L_0, \Delta B_0$  = initial extension of the springs
- $\Delta L, \Delta B$  = extension of the springs under load
- $F_{L0}, F_{B0}$  = prestress force created by  $\Delta L_0, \Delta B_0$
- $F_L, F_B$  = spring force created by  $\Delta L, \Delta B$
- $d$  = deflection of the trampoline centre
- $l, b$  = half length/breadth of the rigid plate

To find an explicit solution of (6) we introduce the following approximations:

From Figure 2 we have

$$F_L = 2(F_{L0} + c\Delta L)\sin \alpha \quad (1)$$

$$\sin \alpha = \frac{d}{L_0 + \Delta L} \quad (2)$$

Introduce

$$F_{L0} = c\Delta L_0 \quad (3)$$

and substitute (2) and (3) in (1)  
we get

$$F_L = 2cd \frac{\Delta L_0 + \Delta L}{L_0 + \Delta L} \quad (4)$$

Using Figure 3 accordingly yields

$$F_B = 2cd \frac{\Delta B_0 + \Delta B}{B_0 + \Delta B} \quad (5)$$

Add Equation (4) and (5) then

$$F = F_L + F_B \quad (6)$$

$$L_0 + \Delta L \approx L_0 \quad (7)$$

$$B_0 + \Delta B \approx B_0 \quad (8)$$

Substitute (4),(5),(7) and (8) in (6) then

$$F \approx 2cd \left[ \frac{(\Delta L_0 + \Delta L)}{L_0} + \frac{(\Delta B_0 + \Delta B)}{B_0} \right] \quad (9)$$

Applying the Pythagorean theorem to either of the rectangular triangles of Fig. 2 and rearranging we obtain

$$\frac{\Delta L}{L_0} = \sqrt{1 + \frac{d^2}{L_0^2}} - 1 \quad (10)$$

Expanding the square root into a Taylor series and using the first two terms leads to

$$\frac{\Delta L}{L_0} \approx \frac{1}{2} \frac{d^2}{L_0^2} \quad (11)$$

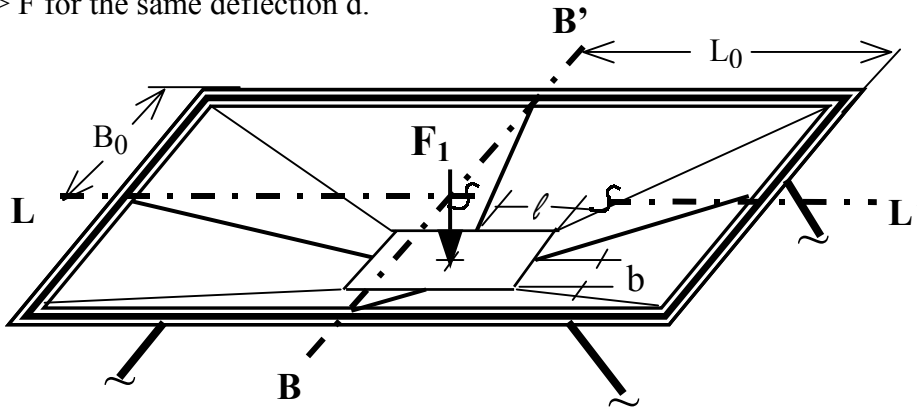
Repeating the same procedure on either of the rectangular triangle of Fig. 3 yields

$$\frac{\Delta B}{B_0} \approx \frac{1}{2} \frac{d^2}{B_0^2} \quad (12)$$

When substituting (11) and (12) in (9) and rearranging, we have

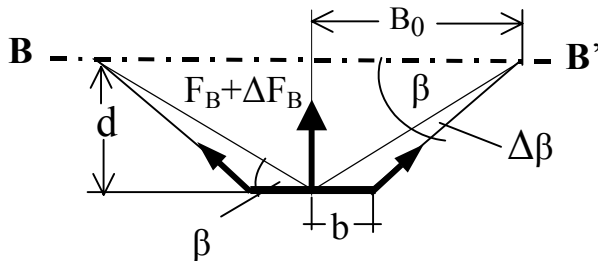
$$F \approx 2c \left( \frac{\Delta L_0}{L_0} + \frac{\Delta B_0}{B_0} \right) d + c \left( \frac{1}{L_0^2} + \frac{1}{B_0^2} \right) d^3 \quad (13)$$

To further improve the models performance, a rigid weightless plate is centrally placed on the trampoline to take the foot contact area of the gymnast into consideration, which causes a force  $F_1 > F$  for the same deflection  $d$ .



**Fig. 4: Trampoline with a weightless rigid plate of an area  $4 b l$  \*)**

Thus the cross-sectional view has changed and is shown in Fig. 5. The modified longitudinal-sectional view can be set up accordingly when changing  $B$  to  $L$ ,  $b$  to  $l$  and  $\beta$  to  $\alpha$ .



**Fig. 5: Cross-sectional view of the modified model**

$$\Delta\beta \ll \beta$$

$\Delta F_B$  = partial increase of the spring force due to the rigid plate

$b$  = half breadth of the plate

**and for the longitudinal view**

$$\Delta\alpha \ll \alpha$$

$\Delta F_L$  = partial increase of the spring force due to the rigid plate

$l$  = half length of the rigid plate

Consequently the increase  $\Delta F$  and the total spring force  $F_1$  for the same deflection  $d$  due to the rigid plate can be calculated as

$$\Delta F = \Delta F_B + \Delta F_L \quad (14) \quad \text{and}$$

$$F_1 \approx F + \Delta F \quad (15) \quad \text{respectively.}$$

### Problems for solution

1. Use Fig. 5 and show that 
$$\Delta F \approx c \left( \frac{\ell}{L_0^3} + \frac{b}{B_0^3} \right) d^3 \quad (16)$$

Combine (13), (15) and (16) and the mathematical model of the vertical spring force  $F_1$  of the trampoline bed with the rigid plate should come out as follows:

$$F_1 \approx 2c \left( \frac{\Delta L_0}{L_0} + \frac{\Delta B_0}{B_0} \right) d + c \left( \frac{1}{L_0^2} + \frac{1}{B_0^2} + \frac{\ell}{L_0^3} + \frac{b}{B_0^3} \right) d^3 \quad (17)$$

- Equation (17) is of the form  $F_1 \approx k_1 d + k_3 d^3$ . Check its plausibility when  $L_0$  and  $B_0$  approaches large values, when  $\ell$  and  $b$  approaches zero and when  $\Delta L_0$  and  $\Delta B_0$  approaches small and large values respectively.
  - Asses the impact of the approximations due to equations (7),(8), (11), (12) and (16) on the mathematical model of equation (17).
  - The validation of the model can be made with experimental measurements at a real trampoline and through a curve fitting procedure. Can this curve fitting procedure compensate for eventual parametrical and structural errors of the model which are due to the applied mathematical approximations?
  - Write down the reasons, why the independent variable  $d$  of equation (17) only has positive odd exponents.
  - Why is it sufficient to solely use the cross-sectional and longitudinal-sectional view of Fig. 2 and Fig. 3 for setting up the mathematical model of Eq. (17) and disregard all the other possible isosceles triangles through  $F$ ?
- \*) Kraft, M.: Eine einfache Näherung für die vertikale Federkraft des Trampolinsprungtuchs.  
( A simple approximation of the vertical spring force of a trampoline bed.)  
<http://opus.tu-bs.de/opus/volltexte/2001/214>